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Applicant(s): RICOH COMPANY, LTD.

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I, Tadahiko Itoh, a Patent Attorney of Tokyo, Japan having my office at 32nd Floor, Yebisu Garden Place Tower, 20-3 Ebisu 4-Chome, Shibuya-Ku, Tokyo 150-6032, Japan do solemnly and sincerely declare that I am the translator of the attached English language translation and certify that the attached English language translation is a correct, true and faithful translation of Japanese Patent Application No. 2001-090711 to the best of my knowledge and belief.

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5 [CLAIM 6]. A semiconductor distributed Bragg reflector  
as claimed in claim 4, wherein a main layer and a  
heterospike relaxation layer constituting said  
10 semiconductor distributed Bragg reflector having a  
carrier density in the range from  $5 \times 10^{17} [\text{cm}^{-3}]$  to  $2 \times 10^{18} [\text{cm}^{-3}]$ , said heterospike relaxation layer having  
a thickness in the range from 5 [nm] to 40 [nm], an  
average change rate of Al composition in said region  
15 II being in the range from  $0.02 [\text{nm}^{-1}]$  to  $0.15 [\text{nm}^{-1}]$ .

[0015]

(6) The invention of claim 6 has a feature  
in that a main layer and a heterospike relaxation  
20 layer constituting said semiconductor distributed  
Bragg reflector of claim 4 have a carrier density in  
the range from  $5 \times 10^{17} [\text{cm}^{-3}]$  to  $2 \times 10^{18} [\text{cm}^{-3}]$ , the  
heterospike relaxation layer has a thickness in the  
range from 5 [nm] to 40 [nm], an average change rate  
25 of Al composition in the region II is in the range  
from  $0.02 [\text{nm}^{-1}]$  to  $0.15 [\text{nm}^{-1}]$ . Here, the Al  
compositional gradient in the region I is defined as  
"Al compositional gradient = {variation (0-1) of Al

content in the region I}/dI". By choosing each  
parameter of the heterospike buffer layer 12 that  
includes the distributed Bragg reflector to the  
foregoing range, reduction of resistance is achieved  
5 easily and effectively.

[0060]

FIG.13 shows the Al composition gradient  
that provides minimum of the electric resistance and  
10 the corresponding sheet differential resistance for  
the case of changing the carrier density of the  
distributed Bragg reflector and the heterospike  
buffer layer 12 ( $5 \times 10^{17} [\text{cm}^{-3}]$ ,  $2 \times 10^{18} [\text{cm}^{-3}]$ ) and  
the thickness of the heterospike buffer layer 12 in  
15 the structure of FIG.6, together with the percentage  
of the electric resistance decrease in comparison  
with the case in which a simple linear compositional  
gradient is used for the heterospike buffer layer  
(the structure of FIG.2).

20

[0061]

In view of increase of electrical  
resistance with decrease of the carrier density, the  
value of  $5 \times 10^{17} [\text{cm}^{-3}]$  is chosen as the actually  
25 allowable lower limit. Further, a value of  $2 \times 10^{18}$   
[ $\text{cm}^{-3}$ ] is chosen as the allowable upper limit in view  
of conspicuous optical absorption particularly in the  
case of a p-type semiconductor.

[0062]

In the case the thickness of the heterospike buffer layer 12 is increased, a remarkable decrease of resistance is achieved. On the other hand, such a decrease of the thickness of the heterospike buffer layer 12 is not preferable in view of decrease of reflectance of the distributed Bragg reflector. From the viewpoint of reflectance, it is believed that the value of 40 [nm] or less is important for the practical thickness of the heterospike buffer layer.

[0063]

In the case the thickness is too small, the desired resistance decrease is not attained. Thus, it is believed that the value of 5 [nm] or more is important for the thickness of the heterospike buffer layer 12 for realizing sufficient resistance reduction effect.

[0064]

As compared with the case of the simple compositional gradation layer in which the Al content is changed linearly from the small-bandgap layer to the large-bandgap layer constituting the main layers of the distributed Bragg reflector, the foregoing construction can achieve further reduction of the

resistance. Within the foregoing range, the differential sheet resistance is decreased to about 75% ( $1.2 \times 10^{-9} [\Omega \text{cm}^2]$  in terms of differential sheet resistance) in the embodiment of claim 3, and thus a significant effect is achieved.

[0065]

Thus, the present embodiment can reduce the resistance further as compared with the case of using the linear compositional gradient in the heterospike buffer layer 12 of the same thickness. In the case of achieving the same resistance value, on the other hand, the present embodiment allows the use of reduced thickness for the necessary heterospike buffer layer 12. Thus, adversary effect on the optical properties such as reflectance is minimized.

Thus, it becomes possible to obtain a distributed Bragg reflector excellent in terms of electric properties and optical properties, by choosing the structure of the distributed Bragg reflector and heterospike buffer layer as set forth in the claims.

[FIG.13]

Heterospike buffer layer thickness	$5 \times 10^{17} [\text{cm}^{-3}]$ carrier density	$2 \times 10^{18} [\text{cm}^{-3}]$ carrier density
5 [nm]	$0.16 [\text{nm}^{-1}] / 8.4 \times 10^{-6} [\Omega \text{cm}^2] / 83\%$	$0.16 / 4.5 \times 10^{-8} [\Omega \text{cm}^2] / 90\%$
40 [nm]	$0.02 [\text{nm}^{-1}] / 2.1 \times 10^{-9} [\Omega \text{cm}^2] / 91\%$	...

